

*Basics
of
Radio Interferometry*

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Second International Convention
Of the *European Radio Astronomy Club*
And the *S.E.T.I. League USA*

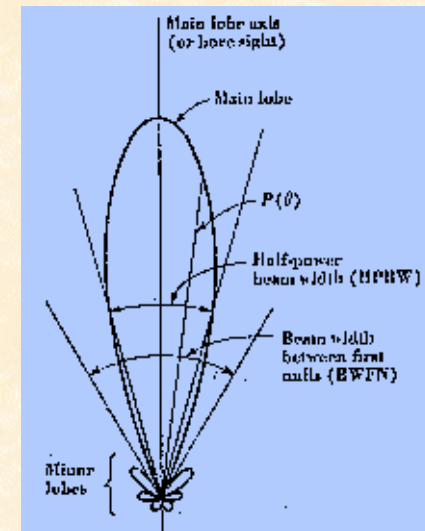
Heppenheim, September 9-10, 2000

What will we talk about?

- Motivation for Radio Interferometry
- Basic Ideas
- The Two-Element Interferometer
(basic interferometer equations)
- Aperture Synthesis
- Amateur Radio Astronomy and Interferometry

Motivation for Radio Interferometry

- angular resolution of a telescope $\propto \lambda/D$
- optical telescopes: 20 marcsec
($D=5\text{m}$, $\lambda=500\text{nm}$)
- radio telescopes: 1 arcmin
($D=100\text{m}$, $\lambda=2.8\text{cm}$)
- extra-galactic radio sources:
fine scale structures < 1 marcsec
($1\text{marcsec @ } \lambda = 2.8\text{cm} \Rightarrow D = 6000\text{km}$)
- filled aperture telescopes limited to $D \approx 100\text{m}$



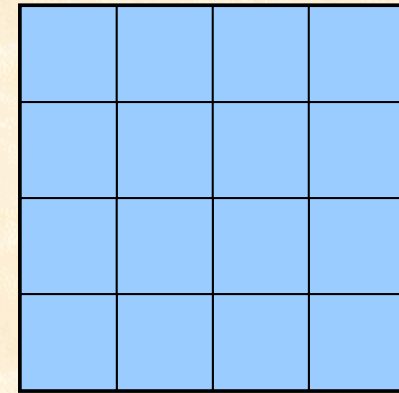
The Solution

- There is a way to build big radio telescopes:
 - take several “small” telescopes in great distance from one another
 - combine their output signals in an appropriate way
 - do some computing on the results

That is a very simplistic view
of a **radio interferometer**

Basic ideas I

- fixed aperture antenna composed from N elemental areas
- each element n is contributing a signal
 $I_n \cos(\omega t + \Phi_n)$
- vectorial addition of all signals yields:

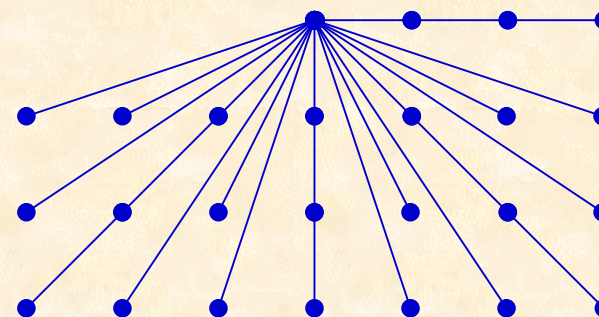
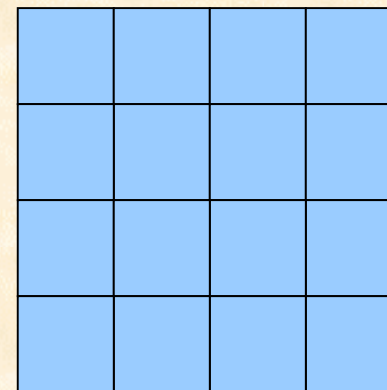


$N = 16$

$$\begin{aligned} P &\propto \frac{1}{2} \cdot \sum_{j=1}^N \sum_{k=1}^N I_j I_k \cos(\Phi_j - \Phi_k) \\ &= \frac{1}{2} \cdot \sum_{j=1}^N I_j^2 + \sum_{j=1}^{N-1} \sum_{k=j+1}^N I_j I_k \cos(\Phi_j - \Phi_k) \end{aligned}$$

Basic Ideas II

- cross terms can be measured separately one pair at a time
- addition to be done later
- two moveable antennas → simulation of a large dish

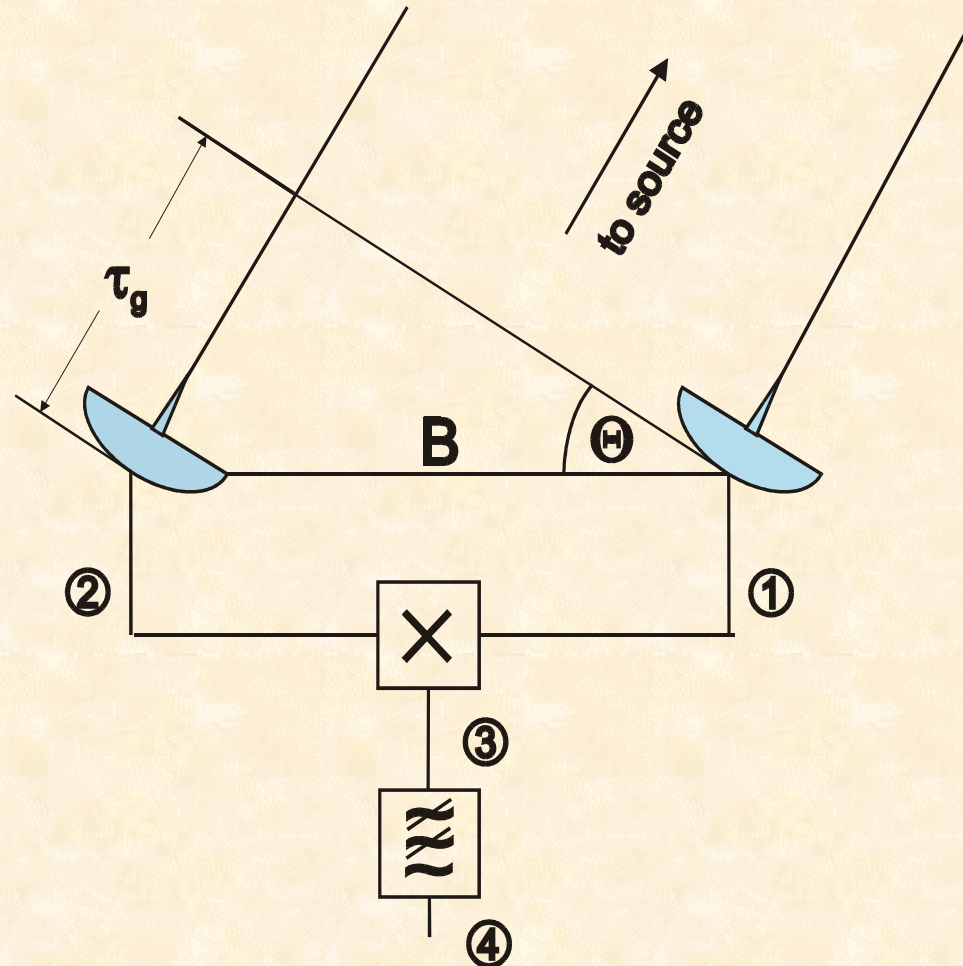


The Two-Element Interferometer I

B = Baseline

Θ = angle between
base line and wave
front from source

$\tau_g = B \cdot \sin \Theta / c$ wave
propagation
(geometric) delay



The Two-Element Interferometer II

- assuming a point source and monochromatic radiation:

① $R_1(t) = E \cdot \cos \omega t$

② $R_2(t) = E \cdot \cos \omega(t - \tau_g)$

③ $R_3(t) = R_1(t) \cdot R_2(t)$

$$= [E \cdot \cos \omega t] \cdot [E \cdot \cos \omega(t - \tau_g)]$$

$$= \frac{1}{2}E^2 \cdot [\cos \omega(t + t - \tau_g) + \cos \omega(t - t + \tau_g)]$$

$$= \frac{1}{2}E^2 \cdot [\cancel{\cos \omega(2t - \tau_g)} + \cos \omega\tau_g]$$

④ $R_4 = \frac{1}{2}E^2 \cdot \cos \omega\tau_g$

The Two-Element Interferometer III

- tracking the source / earth rotation make:

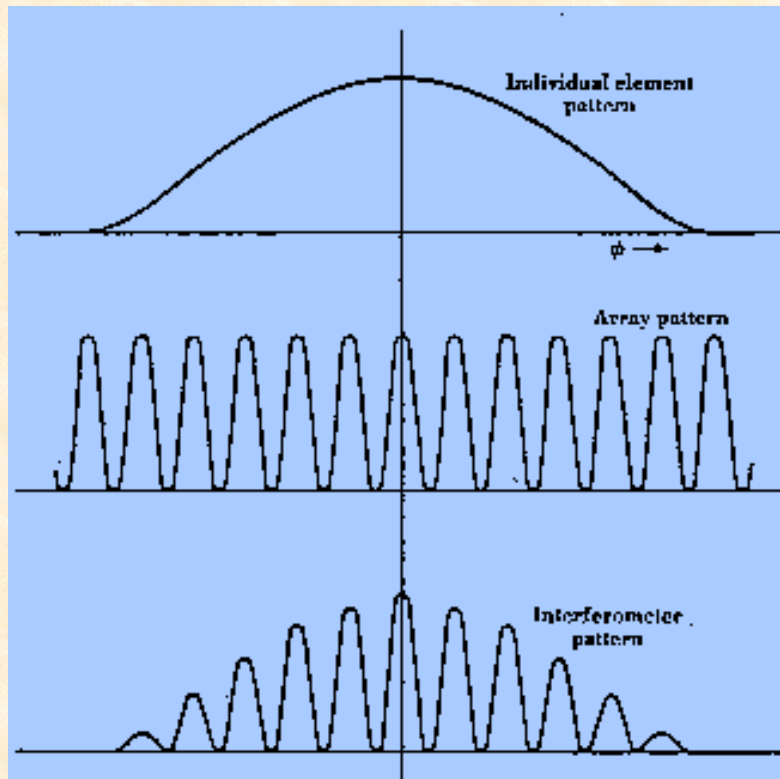
$$\Theta = \Theta(t) \quad \text{and} \quad \tau_g = \tau_g(t) = B \cdot \sin \Theta(t) / c$$

- therefore

$$R_4(t) = \frac{1}{2} E^2 \left[\cos \left(\omega \frac{B \cdot \sin \Theta(t)}{c} \right) \right]$$

$$= \frac{1}{2} E^2 \left[\cos \left(\frac{2\pi B \cdot \sin \Theta(t)}{\lambda} \right) \right] \approx \frac{1}{2} E^2 \cdot \cos \left(\frac{2\pi B \cdot \Theta(t)}{\lambda} \right)$$

The Two-Element Interferometer IV



← single antenna characteristic

← tracking the source

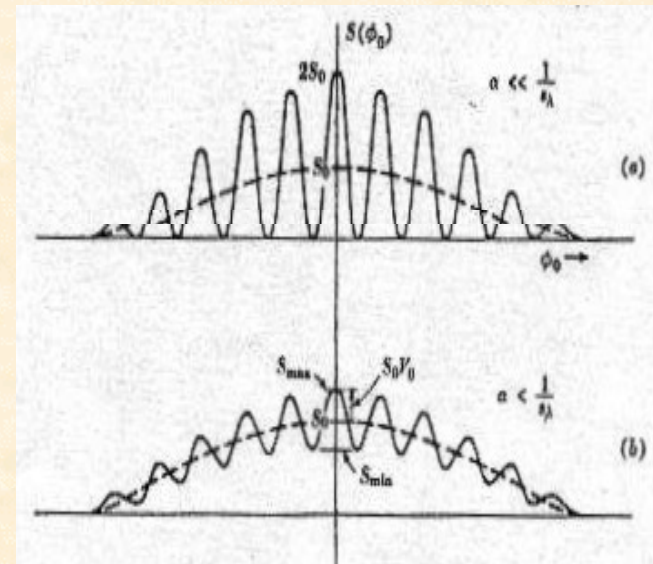
← transit instrument

Requirements for a Working Interferometer

- Technical requirements:
 - local oscillators for mixers of both telescopes phase-locked
 - RF lines from antennas to receivers of equal length
- Radiation requirements
 - planar wave fronts
 - coherence length $\gg \tau_g \cdot c$
 - variation of radiation intensity slow when compared to τ_g

Extended Sources I

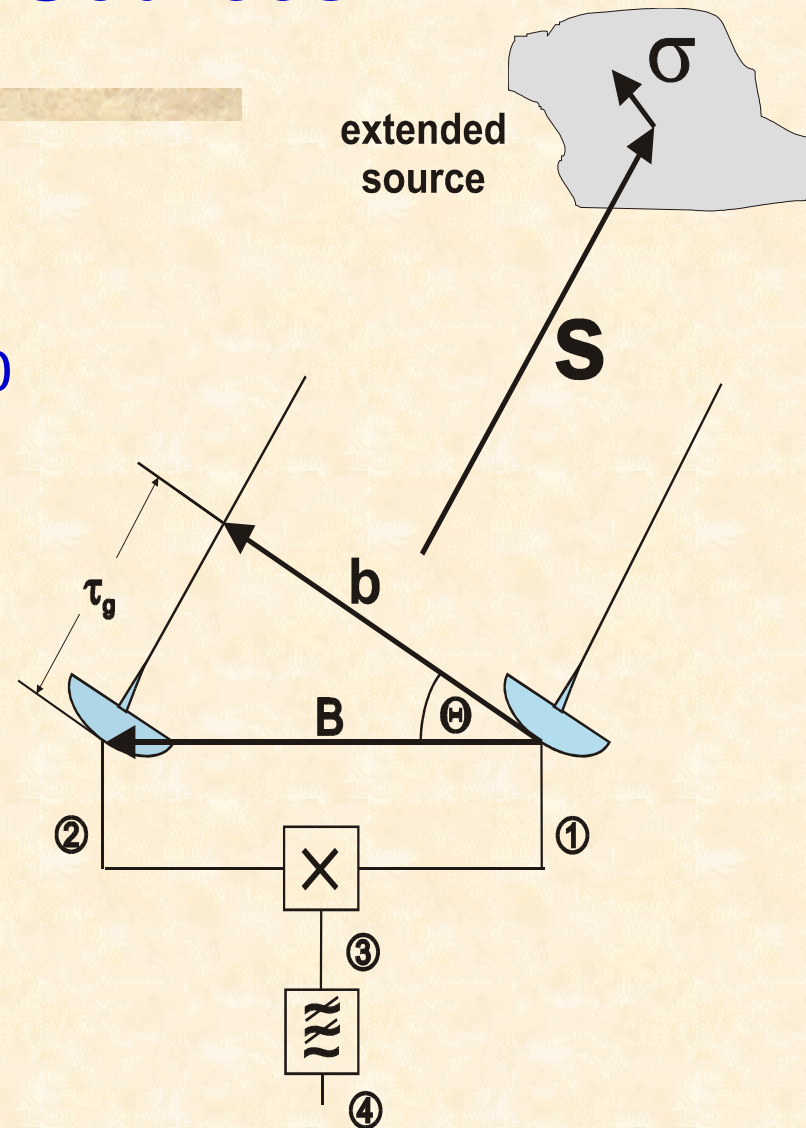
- point source = unrealistic case
- extended source = sum of point sources
- response of the interferometer = sum of the responses to point sources



Extended Sources II

■ using vector notation:

- $\mathbf{s}(t)$ = source vector (to source center)
- σ = element deviation from source center
- \mathbf{B} = vector notation of baseline
- \mathbf{b} = projected spacing



Extended Sources III

$$R(t) \propto \int_{-\infty}^{+\infty} d\boldsymbol{\sigma} \cdot I(\boldsymbol{\sigma}) \cdot \cos(2\pi\mathbf{B} \cdot (\mathbf{s}(t) + \boldsymbol{\sigma}))$$

$$= V \cdot \exp\{i2\pi\mathbf{B} \cdot \mathbf{s}(t)\}$$

$$V = \int_{-\infty}^{+\infty} d\boldsymbol{\sigma} \cdot I(\boldsymbol{\sigma}) \cdot \exp\{i2\pi\mathbf{b} \cdot \boldsymbol{\sigma}\}$$

V = Visibility function = **Fourier transformation of source's brightness distribution**

Bandwidth Effects I

- wide bandwidths desirable → increasing S/N ratio

$$R(t) = \frac{1}{2}E^2 \cdot \cos\left(\frac{2\pi B \cdot \Theta(t)}{\lambda}\right) \quad \text{from monochromatic case becomes:}$$

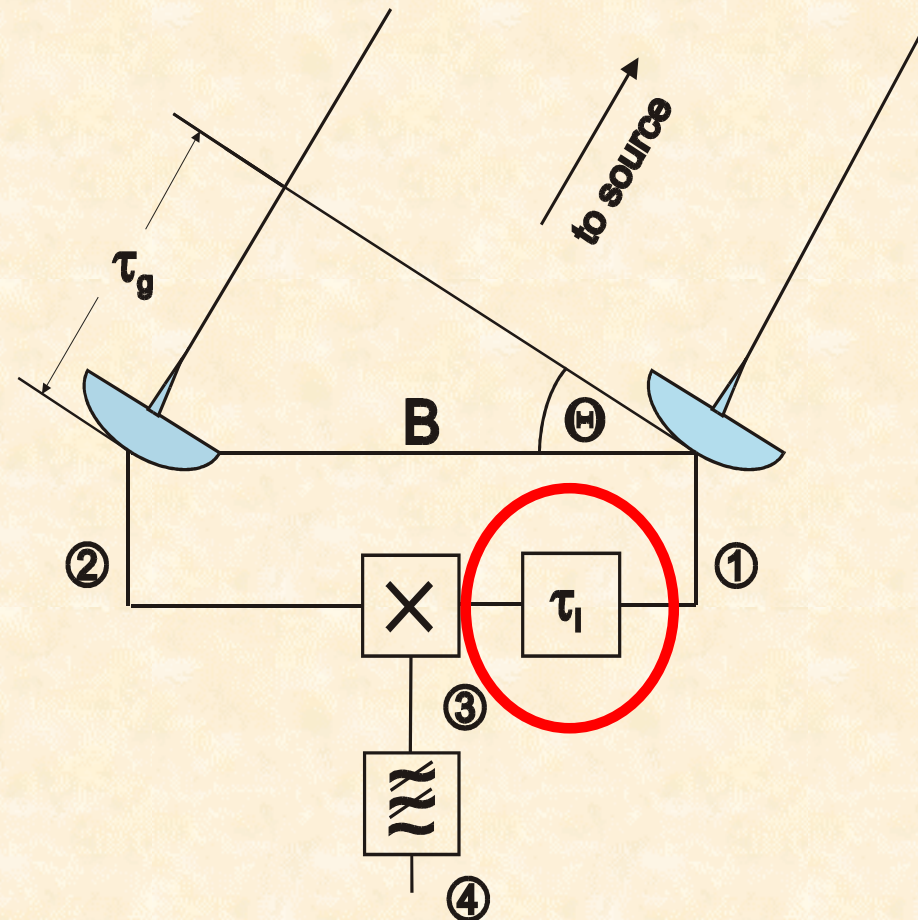
$$R(t) = \frac{1}{2}E^2 \cdot \int_{\omega_0}^{\omega_0 + \Delta\omega} d(\omega) \cdot \alpha(\omega) \cdot \cos\left(\frac{2\pi B \cdot \Theta(t)}{\lambda}\right)$$

$\alpha(\omega)$ = frequency characteristics of equipment

- big $\Delta\omega$: τ_g can lead to loss of correlation !

Bandwidth Effects II

- instrumental delay τ_i for compensation
- exact compensation of τ_g only for \mathbf{s}
- interferences from source elements at $\mathbf{s} + \boldsymbol{\sigma}$



Aperture Synthesis I

- two-element interferometer
 - one Fourier component of brightness distribution
 - measuring at one discrete spatial frequency
- spatial frequency
 - describes how fast the brightness changes with the direction (angle) of observation
 - analogy: frequencies describe how fast the amplitude of an electrical signal changes in time

Aperture Synthesis II

- single radio telescope = low-pass for spatial frequencies
- interferometer = band-pass for spatial frequencies
- reconstruction of brightness distribution needs measuring at many different spatial frequencies
- analogy: voice signal on a phone line
 - one measuring system measures at 1kHz
 - others at 300, 350, ... , 2800, 2900, 3000Hz
 - all together → approximation of the original signal
 - ordinary telephone \cong filled aperture telescope

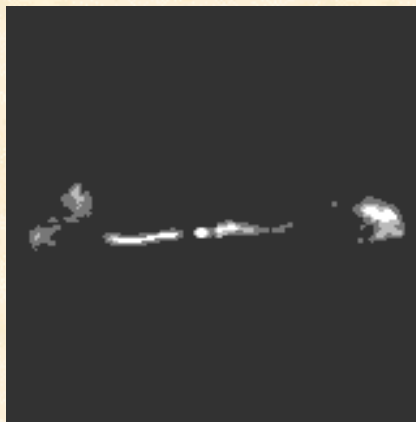
Aperture Synthesis III

Image reconstruction:

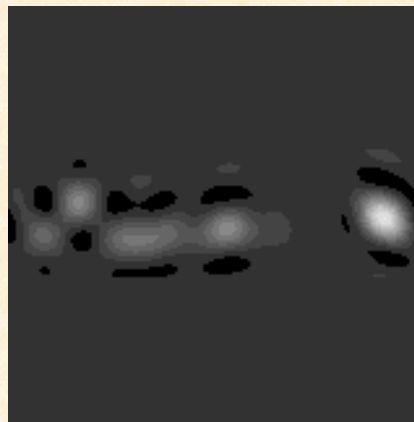
- inverse Fourier transformation of a set of Visibility functions
- cleaning of images necessary
 - CLEAN algorithm (Högbom 1974)
 - variants: Clark, Cotton-Schwab
 - Maximum Entropy Method (Wernecke 1975)

Aperture Synthesis IV

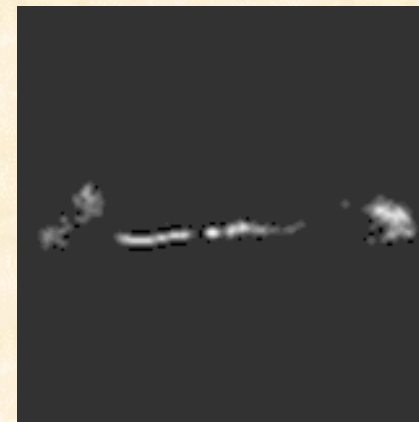
- image quality depends on number of elements



source's
brightness
distribution



9 x 9
components



40 x 40
components

VLBI

- first interferometers: directly connected by RF lines
- not feasible with greater distances
- **Very Long Baseline Interferometry:**
 - inter-continental distances (baselines $> 10000\text{km}$)
 - synchronization of LOs: atomic frequency standards
 - correlation of signals: off-line
 - earth rotation \rightarrow different visibility functions with the same telescopes

Intensity Interferometer

- Hanbury Brown, Twiss (1968)
- interferometer without phase stable system
(incoherent LOs)
- post-detection multiplication
- some correlation due to intensity fluctuations
- low signal-to-noise ratio

Amateur Radio Astronomy and Interferometry I

- lots of amateur radio telescopes available
- main problem: LO and time synchronization
- ALLBIN project:
 - synchronization of time by Astra satellite
 - Phase 1: "only" accumulation of data
 - Phase 2: intensity interferometer (no LO synchronization necessary)
 - Phase 3: ALLBIN a "normal" interferometer ???

Amateur Radio Astronomy and Interferometry II

- What's missing to make ALLBIN a real interferometer?
(Assume data exchange and communication from phase 1 working!)
 - phase 2:
 - understand Intensity Interferometer
 - write software to combine data from telescopes and for imaging
 - phase 3:
 - develop techniques to use satellite signal for LO
 - software (use as much as possible from first step)

Literature I

■ Books

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- Astronomical Optical Interferometry, A Literature Review by Bob Tubbs:
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